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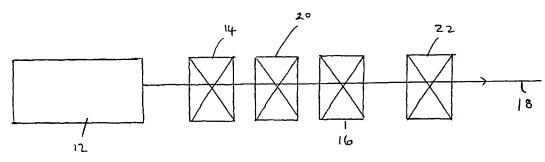
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(54) Title: EXHAUST SYSTEM FOR A DIESEL ENGINE COMPRISING A NO<sub>X</sub>-TRAP



(57) Abstract: An exhaust system (10) for a diesel engine (12) comprises a first NO<sub>X</sub>-trap (16) comprising at least one first NO<sub>X</sub> absorbent and platinum, characterised in that at least one second NO<sub>X</sub> absorbent (14) is disposed upstream of the first NO<sub>X</sub> trap, which at least one second NO<sub>X</sub> absorbent is not associated with platinum

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#### EXHAUST SYSTEM FOR A DIESEL ENGINE COMPRISING A NOx-TRAP

The present invention relates to an exhaust system for a diesel engine, which system comprising a first nitrogen oxide (NO<sub>x</sub>)-trap comprising at least one first NO<sub>x</sub> absorbent and platinum.

Exhaust gases from compression ignition engines, such as diesel engines, comprise a mixture of pollutants including carbon monoxide (CO), unburned hydrocarbons (HC), nitrogen oxides (NO<sub>x</sub>) and particulate matter (PM) including volatile and soluble organic fractions (VOF and SOF respectively). The NO<sub>x</sub> component can comprise nitrogen monoxide (NO) and nitrogen dioxide (NO<sub>2</sub>). The level of these pollutants in exhaust gases from internal combustion engines it is permissible to exhaust to atmosphere is regulated by legislation. Such legislation can be met by engine design, engine management and/or exhaust gas after treatment, and typically a combination of all three measures.

In conventional diesel engines, present legislated limits for HC and CO can be met using a platinum (Pt)-based diesel oxidation catalyst (DOC). Diesel nitrogen oxides (NO<sub>x</sub>) emissions are presently controlled by engine management, such as exhaust gas recirculation (EGR). As a consequence, however, PM emissions including VOF and SOF are increased. The DOC is used to treat VOF and SOF in order to meet presently legislated limits for PM.

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Another prior art exhaust system primarily for treating diesel exhaust comprises an oxidation catalyst for oxidising NO in the exhaust gas to NO<sub>2</sub> and a downstream filter for trapping PM. A process for treating diesel PM that uses this arrangement is described in EP 0341382 or US patent no. 4,902,487, both of which are incorporated herein by reference. The process comprises passing diesel exhaust gas including PM and NO unfiltered over an oxidation catalyst to convert the NO to NO<sub>2</sub>, collecting soot on the filter and combusting the collected soot by reaction with the NO<sub>2</sub>. This technology is commercially available as Johnson Matthey's Continuously Regenerating Trap or CRT<sup>®</sup>. Combustion of the PM in NO<sub>2</sub> results in CO and NO, with a potential side-reaction leading to the complete reduction of the NO<sub>2</sub> to N<sub>2</sub> as described in SAE 890404.

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A problem with the process described in EP 0341382 and in the use of exhaust gas after treatment catalysts such as DOC is that, as exhaust emission legislation is tightened, legislative bodies have begun to discuss limiting the amount of NO<sub>2</sub> it is permissible to exhaust to atmosphere. For example, the California Air Resources Board (CARB) has proposed that a maximum of 20% of tailpipe NO<sub>x</sub> of the relevant drive cycle is emitted as NO<sub>2</sub> (see CARB's Diesel Risk Reduction Program and Final Regulation Order Chapter 14 "Verification procedure, warranty and in-use compliance requirements for in-use strategies to control emissions from diesel engines", section 2706). NO<sub>2</sub> is toxic and can cause headaches, dizziness and nausea in low doses. It also has an objectionable smell. In the process of EP 0341832, if there is insufficient PM on the filter to react with NO<sub>2</sub> generated over the oxidation catalyst or the temperature of the exhaust gas is below a preferred range for combustion of PM in NO<sub>2</sub>, NO<sub>2</sub> can slip past the filter and be undesirably exhausted to atmosphere.

At low exhaust gas temperatures, e.g. about 200-250°C, and part-load, a modern diesel engine produces a relatively high amount of NO<sub>x</sub> in the form of NO<sub>2</sub>. If, as is typical in an exhaust system for a lean-burn internal combustion engine including a NO<sub>x</sub>-trap, the exhaust gas is first passed over a platinum oxidation catalyst, the NO<sub>2</sub> can be removed by facile low temperature oxidation of hydrocarbons present in the exhaust gas. This process is known as lean NO<sub>x</sub> catalysis. In any event, the NO<sub>x</sub> absorbent material can poison the lean NO<sub>x</sub> activity of the platinum, thereby reducing the conversion efficiency of the process. At higher temperatures, e.g. above about 300-350°C, the oxidation of NO to NO<sub>2</sub> becomes sufficiently rapid for significant quantities of NO<sub>2</sub> to be formed and a conventional platinum containing NO<sub>x</sub>-trap then starts to become effective.

A NO<sub>x</sub>-trap is purposely designed for absorbing and storing NO<sub>x</sub> in lean exhaust gases (lambda > 1 conditions), and releasing and catalytically reducing the stored NO<sub>x</sub> in rich exhaust gases (1 > lambda conditions). To remove the stored NO<sub>x</sub>, typically the engine is controlled so that periodically it is run rich during normal lean-running operation. A NO<sub>x</sub>-trap typically includes active materials for three functions: an oxidation catalyst, such as platinum; a NO<sub>x</sub> absorbent, for example a compound of an alkali metal e.g. a potassium and/or a caesium, an alkaline earth compound typified by

barium oxide or a compound of a rare earth metal, such as lanthanum; and a reduction catalyst, such as rhodium. In the exhaust gas the or each alkali metal and alkaline earth metal compound is present as an oxide, although it may also be present in use as a hydroxide or a carbonate.

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A convention used herein is to refer to a "NO<sub>x</sub>-trap" as a composition comprising a NO<sub>x</sub> absorbent and at least one catalytic material, such as a platinum group metal. NO<sub>x</sub> absorbent refers to a material, e.g. alkaline earth metal compound, alkali metal compound or rare earth metal compound, capable of absorbing NO<sub>2</sub> in lean exhaust gas.

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An oxidation catalyst is purposely designed to provide for the reaction of gaseous components with oxygen, typically in as wide a temperature range as possible, especially at lower temperatures. The catalyst oxidises whenever oxygen is available for reaction in the gas stream. Active components of an oxidation catalyst can include platinum, palladium or a base metal active for oxidation such as manganese, copper, molybdenum, cobalt or any other transition element that is active for oxidation.

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An oxygen storage component (OSC) is purposely designed to absorb oxygen from lean exhaust gases and to release oxygen in rich exhaust gas conditions. Examples of suitable OSC include ceria doped with transition metals, e.g. zirconium, or other rare earth metals and manganese-based materials.

According to the present specification, "adsorb" and "absorb" in relation to the storage of NO<sub>x</sub> on suitable basic materials have the same meaning.

Our WO 02/18753 (incorporated herein by reference) describes an exhaust system for a lean-burn internal combustion engine, including a diesel engine, comprising an oxidation catalyst upstream of a NO<sub>x</sub>-trap for oxidising relatively large amounts of unburned hydrocarbons present in exhaust gas in normal lean-running conditions and for oxidising NO in the exhaust gas to NO<sub>2</sub> in lean-running conditions. In one embodiment, a clean-up catalyst comprising an oxygen storage component such as ceria, an oxidation component, such as platinum, a NO<sub>x</sub> reducing component, for example rhodium, and a

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component for suppressing H<sub>2</sub>S, for example NiO, Fe<sub>2</sub>O<sub>3</sub>, MnO<sub>2</sub>, CoO and CrO<sub>2</sub>, is disposed downstream of the NO<sub>x</sub>-trap.

In WO 01/94760, we disclose an exhaust system for a diesel engine comprising a solid NO<sub>x</sub> absorbent for absorbing NO<sub>x</sub> from relatively cool exhaust gas and desorbing adsorbed NO<sub>x</sub> and passing it to atmosphere by intermittently increasing the temperature of the exhaust gas.

We have now found that by using a NO<sub>x</sub>-absorbent which is free of platinum to absorb relatively low temperature engine-derived NO<sub>2</sub> upstream of a NO<sub>x</sub>-trap comprising platinum when the NO<sub>x</sub>-trap is too cool to catalytically reduce the NO<sub>2</sub> to N<sub>2</sub> and to thermally release stored NO<sub>x</sub> when the NO<sub>x</sub> reducing function of the NO<sub>x</sub>-trap is up to temperature, the exhaust system as a whole is able to treat NO<sub>x</sub> more efficiently. More particularly, we have found that the system slips less NO<sub>2</sub> to atmosphere than a system comprising a conventional NO<sub>x</sub>-trap comprising a NO<sub>x</sub> absorbent and platinum as the sole NO<sub>x</sub> absorbent-containing component.

According to one aspect, the invention provides an exhaust system for a diesel engine, which system comprising a first NO<sub>x</sub>-trap comprising at least one first NO<sub>x</sub> absorbent and platinum, characterised in that at least one second NO<sub>x</sub> absorbent is disposed upstream of the first NO<sub>x</sub>-trap, which at least one second NO<sub>x</sub> absorbent is not associated with platinum.

A further advantage of this system over the above-mentioned prior art system is that the system of the invention generates less  $N_2O$  by lean  $NO_x$  catalysis over the platinum component of the first  $NO_x$ -trap.

An aspect of the present invention is the concept of absorbing  $NO_2$  on the second  $NO_x$  absorbent at relatively low temperature when the downstream first  $NO_x$  trap is too cool to catalyse the reduction of  $NO_x$  to  $N_2$ , and thermally releasing the  $NO_x$  when the first  $NO_x$ -trap is up to temperature, e.g. >200°C, such as >225°C, >250°C, >275°C or >300°C.

As is typical for engines including exhaust systems comprising NO<sub>x</sub>-traps, the engine can include an engine control unit (ECU) programmed, in use, intermittently to adjust to the exhaust gas composition to the rich side for regenerating the at least one first NO<sub>x</sub> absorbent.

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Whilst the at least one second NO<sub>x</sub>-absorbent can be associated with a base metal catalyst, e.g. a manganese compound, a cobalt compound or a copper compound, for oxidising nitrogen monoxide (NO) to nitrogen dioxide (NO<sub>2</sub>) in lean exhaust gas or a non-platinum platinum group metal, such as rhodium or iridium for reducing NO<sub>x</sub> to N<sub>2</sub> in rich exhaust gas, or other non-platinum PGMs such as palladium, osmium and ruthenium, preferably the at least one second NO<sub>x</sub>-absorbent is free from components other than the NO<sub>x</sub>-absorbent and optional support.

Each first and second NO<sub>x</sub> absorbent can be selected from alkaline earth metal compounds, alkali metal compounds or rare-earth metal compounds. Suitable alkaline earth metals include calcium, magnesium, strontium and barium. Alkali metals can be potassium and/or caesium and rare earth metals can be cerium, yttrium or praseodymium.

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The first and second NO<sub>x</sub> absorbent can be supported on a suitable support, such as particulate alumina, silica, zirconia, titania, ceria or a mixture or composite oxide according to any two or more thereof, such as ceria-zirconia or alumina-silica

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"Composite oxide" as defined herein means a largely amorphous oxide material comprising oxides of at least two elements which are not true mixed oxides consisting of the at least two elements.

Alternatively, the NO<sub>x</sub>-absorbent can comprise the support e.g. ceria *per se* or alumina *per se*.

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In use, compounds according to the invention can be oxides, although they may be present as nitrates, hydroxides or carbonates in exhaust gas containing  $NO_x$ , CO and  $H_2O$ .

The first NO<sub>x</sub>-trap can be coated on a flow-through monolith, but in one embodiment, it is coated on a particulate filter. In a further embodiment according to the latter aspect, the particulate filter can include a DOC, optionally comprising supported platinum and/or palladium. Alternatively, the first NO<sub>x</sub> trap can be disposed downstream of the filter, which arrangement adopting the process of EP 0341832 and disclosed in EP 0758713.

Optionally there may be a catalyst for oxidising NO to  $NO_2$ , such as platinum on an alumina support, disposed between the at least one second  $NO_x$  absorbent and the first  $NO_x$ -trap as described in our WO 02/18753.

During NO<sub>x</sub>-trap regeneration, pulses of rich exhaust gas can be produced by the engine to convert stored NO<sub>x</sub> to nitrogen. During this process, hydrocarbon or carbon monoxide could pass through the system to atmosphere. To prevent this, the gas downstream of the first NO<sub>x</sub>-trap can be passed over an oxidation catalyst comprising an oxygen storage component, so even if the gas is overall reducing, reductants can still be oxidised, and prevented from entering the atmosphere. In one embodiment, the oxidation catalyst comprises platinum or palladium supported on a bulk ceria-zirconia composite oxide oxygen storage component.

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According to a further aspect, the invention provides a diesel engine, optionally a light-duty diesel engine (as defined by the relevant legislation) comprising an exhaust system according to the invention.

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According to a further aspect the invention provides a flow-through substrate comprising a NO<sub>x</sub>-trap comprising a first zone coated with a composition comprising at least one first NO<sub>x</sub> absorbent and platinum and a second zone coated with a composition comprising at least one second NO<sub>x</sub>-absorbent, which at least one second NO<sub>x</sub> absorbent is not associated with platinum.

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According to a further aspect, the invention provides a method of treating  $NO_x$  in the exhaust gas of a diesel engine, which method comprising (i) absorbing  $NO_2$  from lean exhaust gas in at least one second  $NO_x$  absorbent when a downstream first  $NO_x$ -trap

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comprising at least one first NO<sub>x</sub> absorbent and platinum is inactive for reducing NO<sub>x</sub> using a suitable reductant; (ii) thermally desorbing stored NO<sub>x</sub>; and (iii) reducing thermally desorbed NO<sub>x</sub> on the first NO<sub>x</sub>-trap using a suitable reductant.

In one embodiment, the method comprises the step between steps (i) and (ii) of adsorbing thermally desorbed NO<sub>x</sub> on the at least one first NO<sub>x</sub> absorbent.

In order that the invention may be more fully understood, the following embodiment and Examples are provided by way of illustration only and by reference to the accompanying drawings, in which:

Figure 1 is a schematic diagram of a diesel engine comprising an exhaust system according to the invention;

Figure 2 is a trace of time against NO<sub>2</sub> concentration (ppm) and temperature showing the experimental conditions used in the Examples;

Figure 3 is a trace showing NO<sub>2</sub> adsorption and desorption for a conventional NO<sub>x</sub> trap comprising 5:1 Pt:Pd at a total loading of 120gft<sup>-3</sup>(4.25g litre<sup>-1</sup>);

Figure 3A is a trace showing HC detected downstream of the  $NO_x$  absorbent in the experiment shown in Figure 3;

Figure 4 is a trace showing NO<sub>2</sub> adsorption and desorption for a washcoat component containing Pt at a loading of 80gft<sup>-3</sup>;

Figure 4A is a trace showing HC detected downstream of the NO<sub>x</sub> absorbent in the experiment shown in Figure 4;

Figure 5 is a trace showing NO<sub>2</sub> adsorption and desorption for the washcoat component of the Figure 4 material without platinum;

Figure 5A is a trace showing HC detected downstream of the NO<sub>x</sub> absorbent in the experiment shown in Figure 5.

In the exhaust system 10 shown in Figure 1, 12 is a diesel engine; 14 is a Pt-free NO<sub>x</sub>-trap comprising a second NO<sub>x</sub>-absorbent, e.g. alumina, barium supported on alumina or ceria; 16 is a NO<sub>x</sub>-trap comprising a first NO<sub>x</sub>-absorbent, such as barium supported on alumina, platinum and rhodium; 18 is the exhaust tailpipe. Optional components include an oxidation catalyst 20, such as platinum on alumina, and/or an oxidation catalyst 22 comprising an OSC, such as ceria-zirconium composite oxide.

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We believe that Figure 1 is self explanatory, in combination with the above description.

#### **EXAMPLE 1**

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A ceramic flow through monolith 1.5 inch (38mm) diameter and 3 inches (76mm) long was coated with a conventional NO<sub>x</sub>-trap formulation containing platinum and rhodium at a ratio of 5:1 and total loading of 120gft<sup>-3</sup> (4.25g litre<sup>-1</sup>) and a barium on alumina NO<sub>x</sub>-absorbent. The catalyst was fitted into a standard gas flow rig and a synthetic gas mixture passed over it at a space velocity of 30,000hr<sup>-1</sup>. The gas mixture composition is shown in Table 1 and remained lean for all the tests.

Table 1 Synthetic Gas Mixture used for Tests

Gas	Concentration
NO <sub>2</sub>	200 or 250ppm
СО	0.05%
CO <sub>2</sub>	6%
H <sub>2</sub> O	6%
O <sub>2</sub>	15%
C <sub>3</sub> H <sub>6</sub> (C1)	300ppm
N <sub>2</sub>	Balance

The gas mixture (without NO<sub>2</sub>) flowing through the catalyst was heated to 500°C and held at this temperature for 5 minutes in order to purge the catalyst. The gas was allowed to cool to 120°C and held at this temperature while the NO<sub>2</sub> was added for a period of 5 minutes. The NO<sub>2</sub> was switched off and the gas temperature increased to 500°C for 5 minutes to purge the catalyst (Fig 2). Throughout the test the NO and NO<sub>x</sub>/NO<sub>2</sub> at the outlet to the catalyst was continuously measured so that adsorption (storage) and desorption could be monitored (Fig 3).

From Fig. 3 it can be seen that there was some storage of NO<sub>2</sub> at low temperatures on this NO<sub>x</sub> trap. The majority of the NO<sub>2</sub> entering the catalyst was converted to NO, which was not adsorbed by the storage component in the NO<sub>x</sub> trap. When the temperature was increased NO<sub>x</sub> began to desorb at 430°C and was complete at 500°C. When NO<sub>2</sub> was absent from the gas feed, hydrocarbons (HC) were oxidised over Pt sites, but when the NO<sub>2</sub> was introduced the HC reacted preferentially with it partially reducing it to NO (Fig 3A).

#### **EXAMPLE 2**

A washcoat, containing Pt, was coated onto a monolith, as in Example 1, to give a loading of 2.5g in<sup>-3</sup> (0.15g cm<sup>-3</sup>) with a Pt loading of 80gft<sup>-3</sup> (2.82g litre<sup>-1</sup>) and evaluated as in Example 1. The results (shown in Fig 4) show that NO<sub>2</sub> was not stored at 120°C, but was all converted to NO by reaction with HC (Fig 4A).

#### **EXAMPLE 3**

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The same washcoat, but excluding Pt, as used in Example 2 was coated on the same size monolith to give a loading of 2.5g in<sup>-3</sup> (0.15g cm<sup>-3</sup>) and evaluated in the same way. The results show (Fig 5) that the Pt free washcoat stored NO<sub>2</sub>. Considerably less NO<sub>2</sub> was reduced to NO than with the equivalent washcoat containing Pt, confirmed by the lower HC conversion (Fig 5A). Desorption of NO<sub>x</sub> began as the temperature increased to 350°C.

The results show that the Pt free washcoat system stored the most  $NO_2$  which was then desorbed at a sufficiently high temperature to ensure a Pt containing  $NO_x$  trap fitted downstream would be at its working temperature.

From these results, it appears that Pt free adsorber does not catalyse the reaction between HC and NO<sub>2</sub>, reducing NO<sub>2</sub> to NO, to the same extent as a formulation containing Pt. NO<sub>2</sub> is more easily adsorbed than NO leading to an advantage for NO<sub>2</sub> adsorption of a Pt free adsorber at temperatures where the NO oxidation reaction is slow over Pt.

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Similar results to those shown in Example 3 were obtained from a barium on alumina  $NO_x$  absorbent material.

#### **CLAIMS:**

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- 1. An exhaust system for a diesel engine, which system comprising a first NO<sub>x</sub>-trap comprising at least one first NO<sub>x</sub> absorbent and platinum, characterised in that at least one second NO<sub>x</sub> absorbent is disposed upstream of the first NO<sub>x</sub>-trap, which at least one second NO<sub>x</sub> absorbent is not associated with platinum.
- 2. An exhaust system according to claim 1, wherein each first and second NO<sub>x</sub>-absorbent is selected from the group consisting of alkaline earth metal compounds, alkali metal compounds and rare earth metal compounds.
- 3. An exhaust system according to claim 2, wherein the or each alkaline earth metal is barium, magnesium, strontium or calcium.
- 15 4. An exhaust system according to claim 2, wherein the or each alkali metal is potassium or caesium.
  - 5. An exhaust system according to claim 2, wherein the or each rare earth metal is cerium, yttrium, lanthanum or praseodymium.
  - 6. An exhaust system according to claim 2, 3, 4 or 5, wherein the or each alkaline earth metal compound, the or each alkali metal compound or the or each rare earth metal compound is supported on a support material.
- 7. An exhaust system according to claim 6, wherein the or each support is alumina, silica, titania, zirconia, ceria or a mixture or composite oxide of any two or more thereof.
  - 8. An exhaust system according to claim 6, wherein the NO<sub>x</sub> absorbent comprises the support.
  - 9. An exhaust system according to claim 1, wherein the second  $NO_x$  absorbent is alumina per se.

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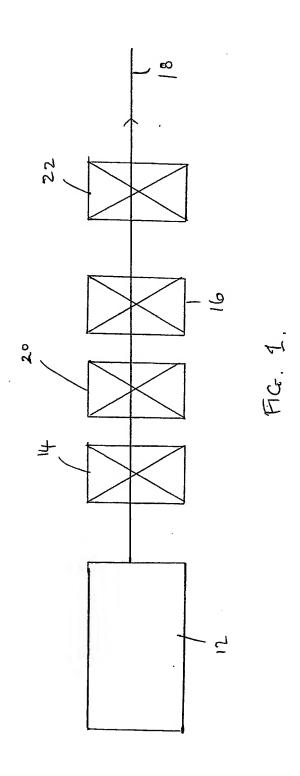
- 10. An exhaust system according to any preceding claim, further comprising a catalyst for oxidising NO to  $NO_2$  disposed between the at least one second  $NO_x$  absorbent and the first  $NO_x$ -trap.
- 5 11. An exhaust system according to claim 10, wherein the NO oxidation catalyst is platinum on an alumina support.
  - 12. An exhaust system according to claim 10 or 11, comprising a particulate filter disposed between the oxidation catalyst and the first NO<sub>x</sub>-trap.
  - 13. An exhaust system according to any of claims 1 to 11, wherein the first NO<sub>x</sub>-trap comprises a particulate filter.
- 14. An exhaust system according to any preceding claim, further comprising a catalyst comprising a catalyst component for oxidising hydrocarbon and carbon monoxide to water and carbon dioxide and an oxygen storage component, which catalyst is disposed downstream of the first NO<sub>x</sub>-trap.
- 15. An exhaust system according to claim 14, wherein the oxidation catalyst comprises platinum or palladium supported on a bulk ceria-zirconia mixed oxide oxygen storage component.
  - 16. A diesel engine comprising an exhaust system according to any preceding claim.
- 25 17. A light-duty diesel engine according to claim 16.
  - 18. An engine according to claim 16 or 17, comprising an engine control unit, when in use, intermittently to adjust the exhaust gas composition to the rich side for regenerating the at least one first  $NO_x$  absorbent.
  - 19. A flow-through substrate comprising a NO<sub>x</sub>-trap comprising a first zone coated with a composition comprising at least one first NO<sub>x</sub> absorbent and platinum and a

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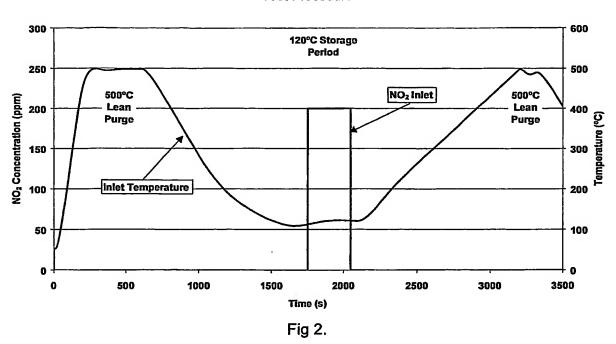
second zone coated with a composition comprising at least one second NO<sub>x</sub>-absorbent, which at least one second NO<sub>x</sub> absorbent is not associated with platinum.

20. A method of treating NO<sub>x</sub> in the exhaust gas of a diesel engine, which method comprising (i) absorbing NO<sub>2</sub> from lean exhaust gas in at least one second NO<sub>x</sub> absorbent when a downstream first NO<sub>x</sub>-trap comprising at least one first NO<sub>x</sub> absorbent and platinum is inactive for reducing NO<sub>x</sub> using a suitable reductant; (ii) thermally desorbing stored NO<sub>x</sub>; and (iii) reducing thermally desorbed NO<sub>x</sub> on the first NO<sub>x</sub>-trap using a suitable reductant.

21. A method according to claim 20, comprising the step between steps (i) and (ii) of adsorbing thermally desorbed NO<sub>x</sub> on the at least one first NO<sub>x</sub> absorbent.



#### **Test Procedure**



NO<sub>2</sub> Adsorption and Desorption for Conventional NOx-Trap 120/5:0:1

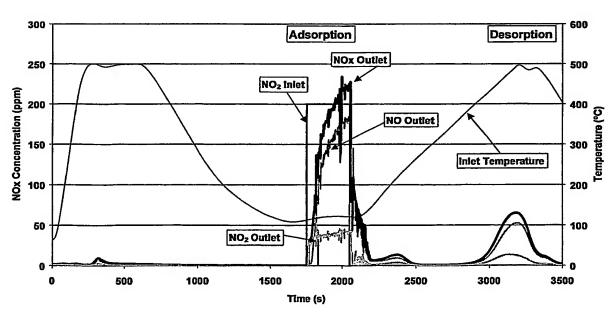
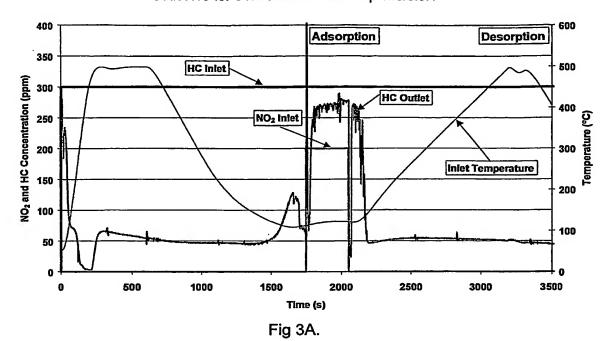
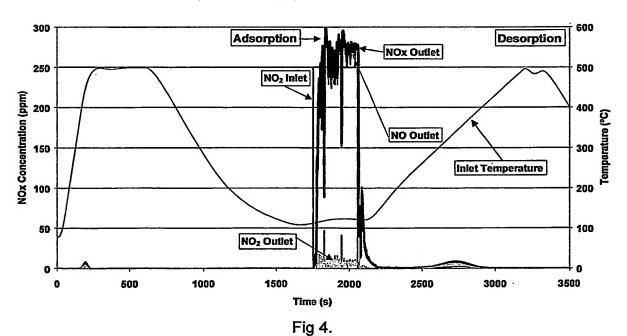


Fig 3.

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Outlet HC for Conventional NOx-Trap 120/5:0:1



NO<sub>2</sub> Adsorption and Desorption for Pt Containing Washcoat



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#### Outlet HC for Pt Containing Washcoat

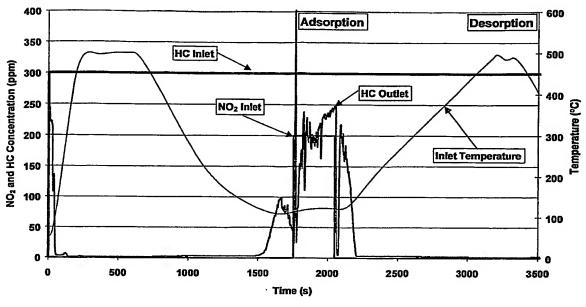


Fig 4A.

#### NO<sub>2</sub> Adsorption and Desorption for Washcoat minus Pt

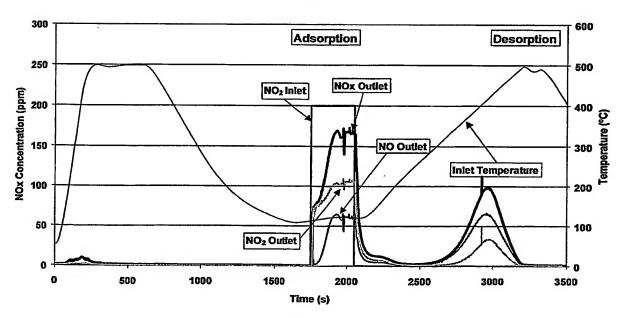
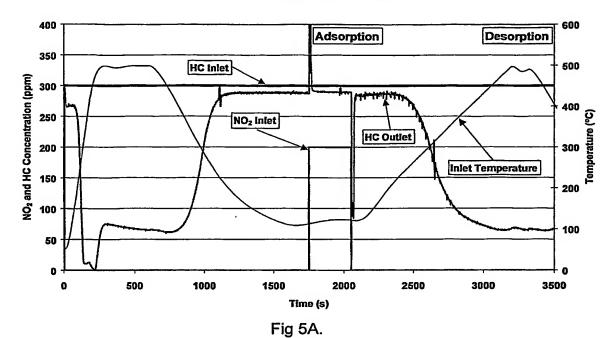


Fig 5.

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Outlet HC for Washcoat minus Pt





Internat | Application No PCT/up 03/04290

A. CLASSIFICATION OF SUBJECT MATTER IPC 7 B01D53/94 F01N3/08

According to International Patent Classification (IPC) or to both national classification and IPC

#### B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols) IPC 7 B01D F01N

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, WPI Data, PAJ

	INTS CONSIDERED TO BE RELEVANT	<del></del>
Category °	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	EP 0 893 154 A (VOLKSWAGENWERK AG) 27 January 1999 (1999-01-27) column 3, line 6 - line 53; figure 1	1-8,10, 11,14-21
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X Further documents are listed in the continuation of box C.	Patent family members are listed in annex.
Special categories of cited documents:  A document defining the general state of the art which is not considered to be of particular relevance  E earlier document but published on or after the international filling date  L document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another claim or other special reason (as specified)  O document referring to an oral disclosure, use, exhibition or other means  P document published prior to the international filling date but later than the priority date claimed	<ul> <li>"T" later document published after the international filing date or priority date and not in conflict with the application but clied to understand the principle or theory underlying the invention</li> <li>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone</li> <li>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.</li> <li>"&amp;" document member of the same patent family</li> </ul>
Date of the actual completion of the international search 20 January 2004	Date of mailing of the international search report  27/01/2004
Name and malling address of the ISA  European Patent Office, P.B. 5818 Patentlaan 2  NL – 2280 HV Rijswijk  Tel. (+31–70) 340–2040, Tx. 31 651 epo ni,  Fax: (+31–70) 340–3016	Authorized officer  Eijkenboom, A

## INTERNATIONAL SEARCH REPORT

Internat Application No
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